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# **STORMWATER MANAGEMENT REPORT**

## **PROPOSED 3-PLEX**

12 VICTORIA AVENUE WEST (CREDITON)

Municipality of South Huron, County of Huron

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## **1. Introduction**

An existing 2 storey Triplex exists at 12 Victoria Ave West (Crediton) in the Municipality of South Huron. The 0.11 Hectare property is on the North side of Victoria Ave. The existing Triplex is to remain, and the construction of a new Triplex building (18.0m x 8.5m) is being proposed to the North of the existing building.

MTE Surveyors have surveyed the lot line orientations and dimensions. BOS Engineering & Environmental Services Inc. (BOS) has surveyed spot elevations and acquired all necessary information in order to create a development plan for both stormwater and sanitary servicing of the lot.

The entire property drains towards the Northeast corner of the lot.

BOS Engineering and Environmental Services Inc. (BOS) undertook a stormwater assessment of the property. The purpose was to provide drainage of the site in accordance with municipal requirements. It was also necessary to provide temporary on-site storage of appropriate storm water detention volumes to control water quality and to limit peak flows from the site to the 5-year predevelopment condition.

The stormwater management system requirements are summarized in this report and on Drawing S-1 in Appendix B.

## **2. Procedure**

The procedure included the following steps:

1. Create base plan with site elevation survey and develop elevation contours and drainage directions.
2. Prepare site/servicing plan with building footprints and servicing assumptions and locations.
3. Assess local rainfall Intensity Duration and Frequency (IDF) data (MTO)
4. Calculate peak 5-year pre-development flows using the "Rational Method"
5. Size outflow structure, piping and slopes
6. Estimate required detention storage volume using the "Modified Rational Method"
7. Design of proposed ponding areas, grades and swales relating to construction.
8. Preparation of report and drawing.

### **3. Findings**

Table 1 in Appendix A identifies the IDF curve as georeferenced from Ministry of Transportation Ontario for the Crediton area.

Table 2 in Appendix A identifies the lot area as 1063 m<sup>2</sup>. Based on cover factors, the lumped runoff coefficient was calculated to be 0.65.

As calculated in Table 3, the maximum grade differential across the site is approximately 0.20m over 64m toward the northeast. The 5-year pre-development flow is 3.66 L/s which requires a 36 mm diameter orifice to regulate the flow and a 150mm diameter outlet pipe at 1.0% minimum slope.

From Tables 4 & 5 in Appendix A, the volume of required storage for the 5 year and 100-year post-development storms respectively are 11.0 m<sup>3</sup> and 22.8 m<sup>3</sup>.

The available storage is rectangular as identified on the servicing plan in Appendix B with a ponding volume of approximately 32.5 m<sup>3</sup>.

Hence, the ponding area is sufficient to store the entire difference between the 5-year post-development and predevelopment storms. It will also store 100% of the difference between the 100 year post-development storm and the 5-year pre-development storm.

## **5. Stormwater Management Plan**

The proposed stormwater management system provides peak flow attenuation for the 5-year post-development flow and the 100-year post development flow. All excess runoff can be stored on the site based on controlled flow to the 5-year pre-development flowrate.

As a residential lot, the development is not expected to have significant water quality impacts. Much of the site runoff will be through grassed swales. However, the period of construction will require disturbance of soil and possible erosion and silt runoff. Therefore, installation and maintenance of temporary silt control measures is recommended during construction, as outlined on the drawing notes. It is recommended that the outlet structure and ponding area is constructed first and that the catch basins be covered with geotextile until potential silt movement is no longer a threat at this site.

Respectfully Submitted,

**BOS Engineering and Environmental Services Inc.**



**A. W. Bos P. Eng.**

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- Appendix A – Calculations – Tables 1, 2, 3, 4, & 5
- Drawing S-1 (Larger Copy Accompanying)

## APPENDIX A – Calculations

**TABLE 1 - IDF CURVE DATA -Crediton ON**

Based on geo-referenced MTO IDF Curves (2010)

<b>Time (min)</b>	<b>Rainfall Intensity (mm/hr)</b>	
	<b>5 yr</b>	<b>100 yr</b>
<b>5</b>	174.9	291.4
<b>10</b>	107.8	179.5
<b>15</b>	81.2	135.2
<b>30</b>	50.0	83.3
<b>60</b>	30.8	51.3
<b>120</b>	19.0	31.6
<b>360</b>	8.8	14.7
<b>720</b>	5.4	9.0
<b>1440</b>	3.3	5.6

**TABLE 2 : C- Factor Weighting and Areas**

<b><u>PRE-DEVELOPMENT</u></b>	
Runoff Coefficient ( $C_g$ ):	0.25      unitless
Total Area ( $m^2$ ):	1063 $m^2$
Total Area (ha):	0.11      ha
<b><u>POST-DEVELOPMENT</u></b>	
Grass Area ( $A_{gr}$ ):	408 $m^2$
Grass Runoff Coefficient ( $C_g$ ):	0.25      unitless
Impervious (ie.Asphalt,Building,Concrete) Area ( $A_{it}$ ):	655 $m^2$
Impervious Runoff Coefficient ( $C_i$ ):	0.90      unitless
Gravel Area ( $A_{gr1}$ ):	0 $m^2$
Gravel Runoff Coefficient ( $C_{gr}$ ):	0.70      unitless
Weighted Runoff Coefficient ( $C_1$ ):	0.65      unitless
$C_1 = (A_{gr} * C_g + A_{gr1} * C_{gr} + A_{it} * C_i) / (A_{gr} + A_{gr1} + A_{it})$	
Total Area ( $m^2$ ):	1063 $m^2$
Total Area (ha):	0.11      ha

**TABLE 3 - PREDEVELOPMENT FLOW REQUIREMENTS (5-YR) or available outflow**

Using the 5-year return data from Table 1

**COMPOSITE AREA - PRE DEVELOPMENT (C =0.25)**

Runoff Coefficient = 0.25 for predevelopment

DURATION	INTENSITY (mm/hr)	QPRE A x C (COMPOSITE) (ha)	QPRE A x C x I (L/s)
5	174.9	0.027	13.22
10	107.8	0.027	8.15
15	81.2	0.027	6.14
30	50.0	0.027	3.78
32.5	48.4	0.027	3.66
60	30.8	0.027	2.33
120	19.0	0.027	0.67
360	8.8	0.027	0.67
720	5.4	0.027	0.41
1440	3.3	0.027	0.25

**TIME OF CONCENTRATION Using FAA Method**

$$T_c = 1.8 (1.1 - C) L^{0.5} S^{-0.333}$$

L (longest flow path) =	210 ft	64 m
C =	0.25	(Predevelopment Condition)
Slope =	0.003	Slope = (0.20 m over 64m)
tc =	32.5 min.	

THEREFORE ASSUME DURATION = 32.5 min. THEN PREDEVELOPMENT 5-YEAR FLOW =3.66 L/s  
OUTFLOW WILL BE RESTRICTED TO 3.58 L/s using a 36 mm dia. Orifice as per calculation below:

**PROPOSED RESTRICTION - Orifice on outlet of new STM CBMH 1**

Cd =	0.6	unitless
Dia. =	1.42	in (36 mm)
Area =	1.6	in <sup>2</sup>
Area =	0.01	ft <sup>2</sup>
g =	32.17	
H =	5.71	ft (254.30 - 252.56) = 1.74 m
Q =	0.13	ft <sup>3</sup> /s
Q =	0.004	m <sup>3</sup> /s
Q =	3.58	L/s

**Manning's Formula for Outlet Pipe Size:**

Diameter:	0.150	m
Slope:	1.000	%
Mannings "n" :	0.012	unitless
X-sectional Area (A):	0.018	m <sup>2</sup>
Wetted Perimeter (P):	0.471	m
Hydraulic Radius (R):	0.038	m
Flow Capacity (Q=1/nA(R <sup>4/3</sup> )(S <sup>0.5</sup> )):	0.016	m <sup>3</sup> /s
Flow Capacity:	16.5	L/s

Therefore a 150mm diameter PVC outlet @ min. 1.0% slope will exceed orifice flow for predevelopment flowrate.



**TABLE 4 - FLOW STORAGE REQUIREMENTS (5 - YR )**

**COMPOSITE AREA - POST DEVELOPMENT (C=0.65)**

DURATION (min)	INTENSITY (mm/hr)	QPOST A x C (COMPOSITE) (ha)	QPOST A x C x I (L/s)	STORM VOLUME (L)	OUTFLOW RATE (L/s)	RELEASE VOLUME (L)	REQUIRED STORAGE (L)	REQUIRED STORAGE m <sup>3</sup>
5	174.9	0.0691	34	10151.9	3.58	1074	9077.9	9.1
10	107.8	0.0691	21	12514.3	3.58	2148	10366.3	10.4
15	81.2	0.0691	16	14139.5	3.58	3222	10917.5	10.9
30	50	0.0691	10	17413.2	3.58	6444	10969.2	11.0
60	30.8	0.0691	6	21453.1	3.58	12888	8565.1	8.6
120	19	0.0691	4	26468.1	3.58	25776	692.1	0.7
360	8.8	0.0691	2	36776.7	3.58	77328	-40551.3	-40.6
720	5.4	0.0691	1	45135.0	3.58	154656	-109521.0	-109.5
1440	3.3	0.0691	1	55165.0	3.58	309312	-254147.0	-254.1

The required storage volume for the 5-year storm is 11.0 m3.

32.5 m<sup>3</sup> is available - SEE DRAWING

**TABLE 5 - FLOW STORAGE REQUIREMENTS (100 - YR )**

**COMPOSITE AREA - POST DEVELOPMENT (C=0.65)**

DURATION (min)	INTENSITY (mm/hr)	QPOST A x C/(COMPOSITE) (ha)	QPOST A x C x I (L/s)	STORM VOLUME (L)	OUTFLOW RATE (L/s)	RELEASE VOLUME (L)	REQUIRED STORAGE (L)	REQUIRED STORAGE $m^3$
5	291.4	0.0691	56	16914.0	3.58	1074	15840.0	15.8
10	179.5	0.0691	35	20837.8	3.58	2148	18689.8	18.7
15	135.2	0.0691	26	23542.6	3.58	3222	20320.6	20.3
30	83.3	0.0691	16	29010.4	3.58	6444	22566.4	22.6
60	51.3	0.0691	10	35731.9	3.58	12888	22843.9	22.8
120	31.6	0.0691	6	44020.6	3.58	25776	18244.6	18.2
360	14.7	0.0691	3	61433.8	3.58	77328	-15894.2	-15.9
720	9.0	0.0691	2	75225.0	3.58	154656	-79431.0	-79.4
1440	5.6	0.0691	1	93613.4	3.58	309312	-215698.6	-215.7

The required storage volume for the 100-year storm is 22.8 m<sup>3</sup>.

32.5 m<sup>3</sup> is available - SEE DRAWING

## APPENDIX B – Servicing Plan

